



LIRMM

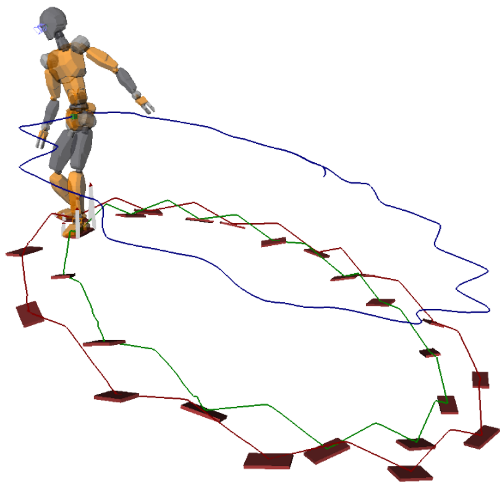
PENDULAR MODELS FOR WALKING OVER ROUGH TERRAINS

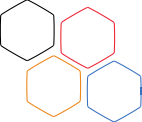
Stéphane Caron

Presentation at Università di Roma "La Sapienza"

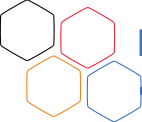
October 19, 2017







Standard model reduction



Multi-body systems

Equation of motion

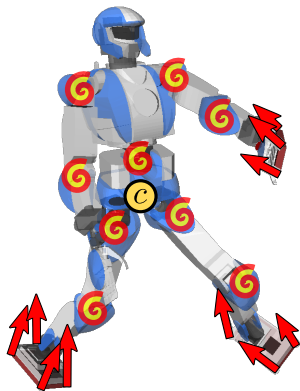
$$M\ddot{q} + h(q, \dot{q}) = S^T \tau + J_c^T F$$

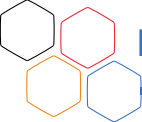
Constraints

- $\tau \in \{\text{feasible torques}\}$
- $F \in \{\text{feasible contact forces}\}$

Assumption

- (Rigid bodies)





Newton-Euler dynamics

Equations of motion

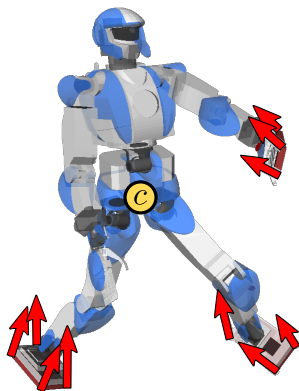
$$\ddot{c} = \frac{1}{m} \sum_i f_i + \vec{g}$$
$$\dot{L}_c = \sum_i (p_i - c) \times f_i$$

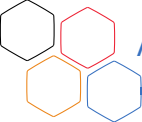
Constraints

- Friction cones: $\forall i, f_i \in \mathcal{C}_i$

Assumption

- Infinite torques



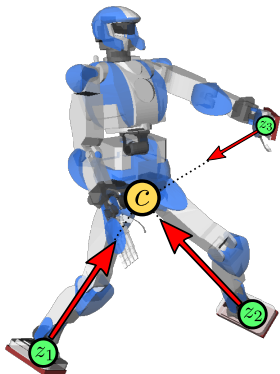


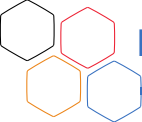
Pendular mode

$$\dot{L}_c = 0$$

Conserve the angular momentum at the center-of-mass

- **Pro:** enables exact forward integration
- **Con:** assumes $\dot{L}_c = 0$ feasible regardless of joint state





Linear Inverted Pendulum Mode

Equation of motion

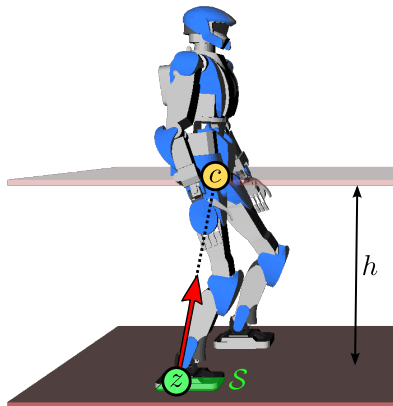
$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

Constraints

- ◆ ZMP support area: $z \in \mathcal{S}$

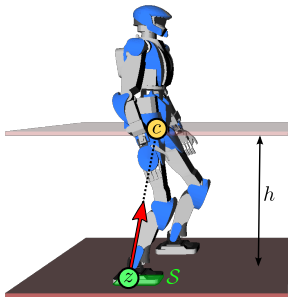
Assumptions

- ◆ Infinite torques
- ◆ Pendular mode $\dot{L}_c = 0$
- ◆ COM lies in a plane: $c_z = h$
- ◆ *Infinite friction*
- ◆ *Contacts are coplanar*



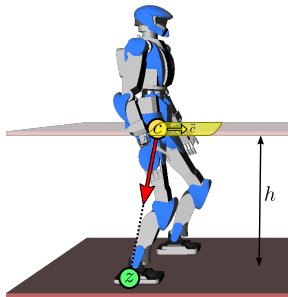
LIPM and CART-table

LIPM [Kaj+01]

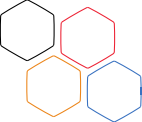


- Input: $z \in \mathcal{S}$
- Output: \ddot{c}

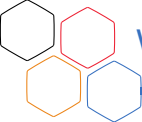
CART-table [Kaj+03]



- Input: $\ddot{c} \in \omega^2(c - \mathcal{S}) + \vec{g}$
- Output: z



Polyhedral geometry: a tool for model reduction



Without infinite friction

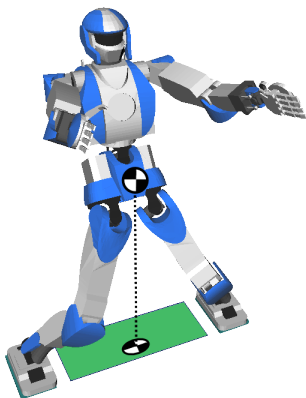
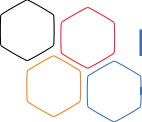
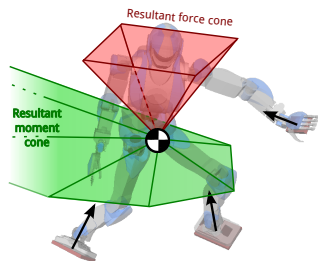


Figure : ZMP support area with friction [CPN17]



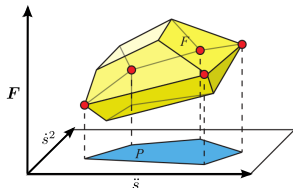
Geometric tool

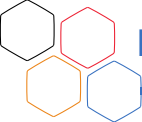
- Apply linear maps to cones
- Project system constraints as support areas / volumes
- Construct *feasibility certificates* for reduced models



Algorithms and ressources

- Double description [FP96]
- Fourier-Motzkin elim. [Zie95]
- Polytope projection [JKM04]
- My website ;) [Car17]





How many contact points per contact?

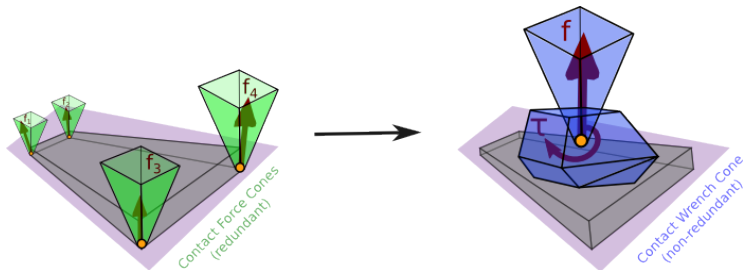
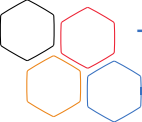


Figure : Reduce redundant friction cones into wrench cones [CPN15]



Torque-limited friction cones

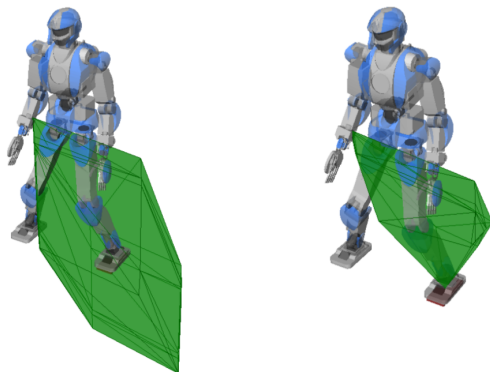
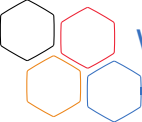


Figure : Friction cones that include actuation limits [Sam+17]



Without coplanar contacts

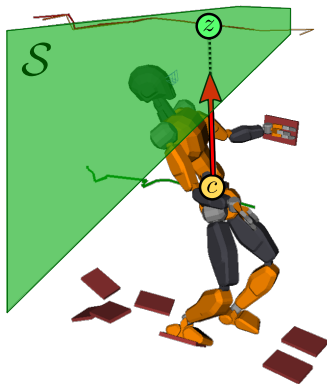
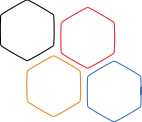


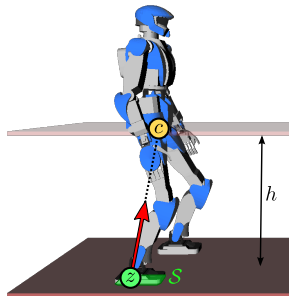
Figure : ZMP support area with non-coplanar contacts [CPN17]



From 2D to 3D locomotion

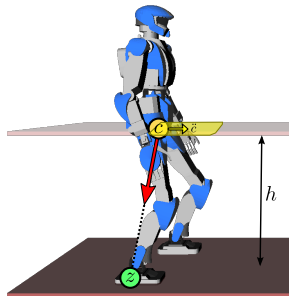
LIPM and CART-table

2D LIPM

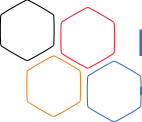


- Input: $z \in \mathcal{S}$
- Output: \ddot{c}

2D CART-table



- Input: $\ddot{c} \in \omega^2(c - \mathcal{S}) + \vec{g}$
- Output: z



Linear Pendulum Mode

Equation of motion

$$\ddot{c} = \text{sign}(h) \omega^2 (c - z) + \vec{g}$$

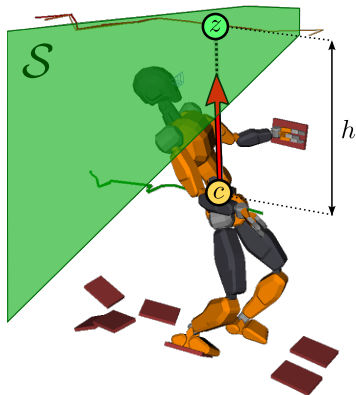
Constraints

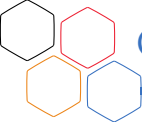
- ◆ ZMP support area: $z \in \mathcal{S}$

Assumptions

- ◆ Inf. torques & pendular mode
- ◆ COM and ZMP lie in parallel virtual planes distant by h

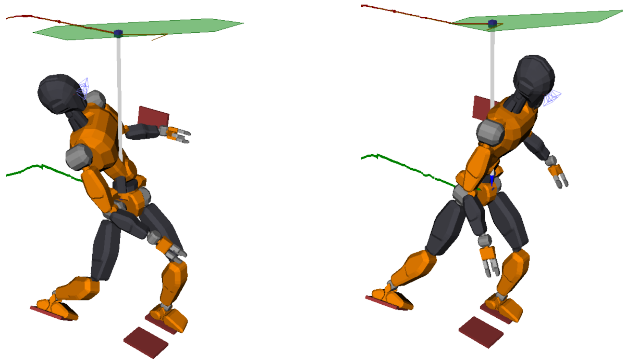
Note: COM is attractor or repulsor depending on $\text{sign}(h)$

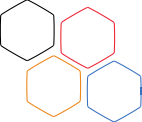




Observation

ZMP support area S changes with COM position:





3D CART-table

Algorithm [CK16]

Compute the 3D cone \mathcal{C} of COM accelerations

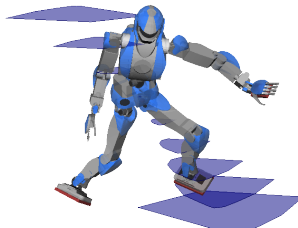


Figure : ZMP support areas for different values of $\pm\omega^2$

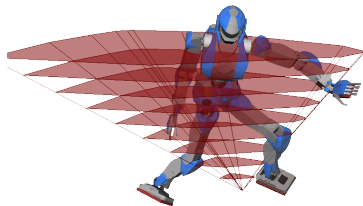
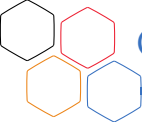
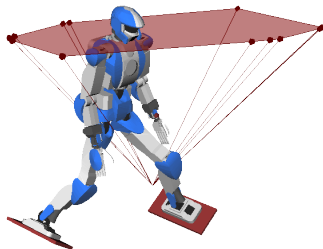
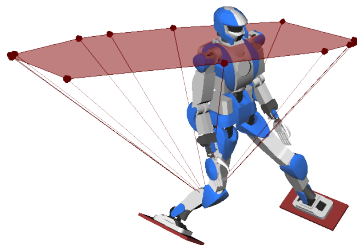


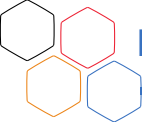
Figure : COM acceleration cone for the same stance



Observation

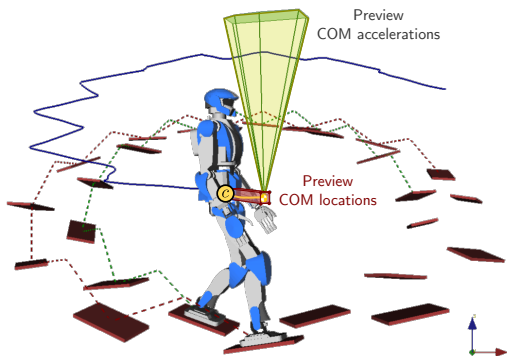
The cone \mathcal{C} still depends on the COM position c :



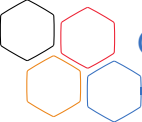


Predictive Control

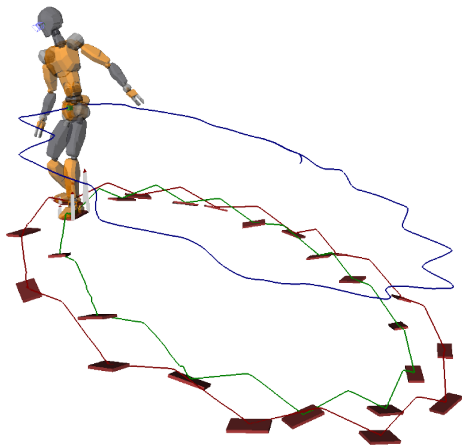
Intersect cones \mathcal{C} over all $c \in \text{preview}$:



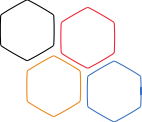
Walking patterns *not very dynamic*, but works surprisingly well!



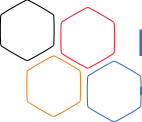
Check it out!



<https://github.com/stephane-caron/3d-com-lmpc>

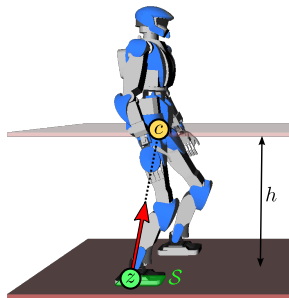


3D Pendulum Mode



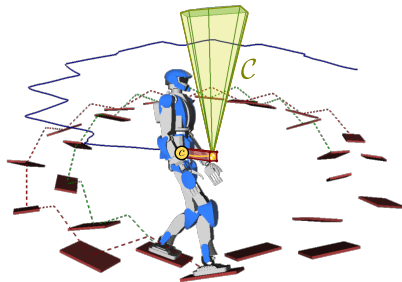
LIPM and CART-table

2D LIPM

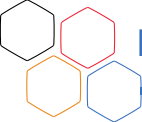


- Input: $z \in \mathcal{S}$
- Output: \ddot{c}

3D COM-accel [CK16]



- Input: $\ddot{c} \in \mathcal{C}(c)$
- Output: z



Inverted Pendulum Mode

Linear Inverted Pendulum

$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

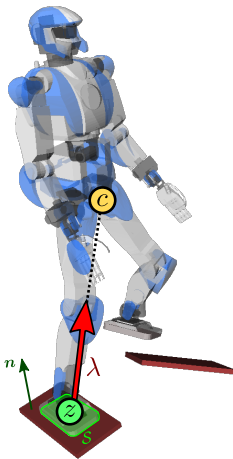
Plane assumption: $\omega = \sqrt{\frac{g}{h}}$

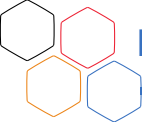


Remove this assumption:

Inverted Pendulum

$$\ddot{c} = \lambda(c - z) + \vec{g}$$





Inverted Pendulum Mode

Equation of motion

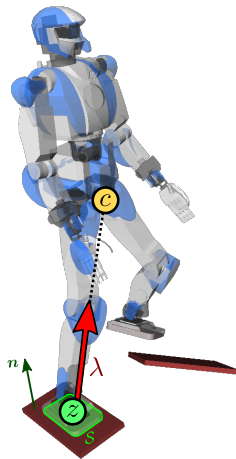
$$\ddot{c} = \lambda(c - z) + \vec{g}$$

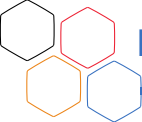
Constraints

- Unilaterality $\lambda \geq 0$
- ZMP support area: $z \in \mathcal{S}$

Assumptions

- Infinite torques
- Infinite friction*
- Pendular mode





Inverted Pendulum Mode with Friction

Equation of motion

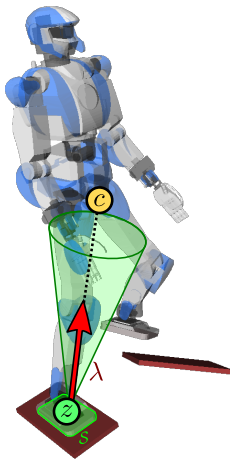
$$\ddot{c} = \lambda(c - z) + \vec{g}$$

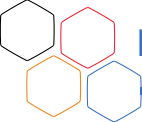
Constraints

- Unilaterality $\lambda \geq 0$
- ZMP support area: $z \in \mathcal{S}$
- Friction: $c - z \in \mathcal{C}$

Assumptions

- Infinite torques
- Pendular mode



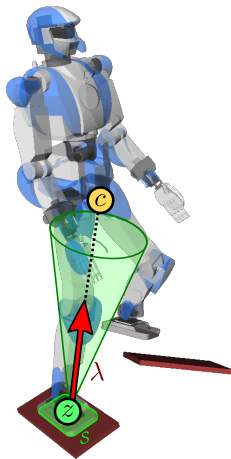


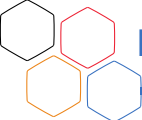
Inverted Pendulum Mode: Question

Equation of motion

$$\ddot{c} = \lambda(c - z) + \vec{g}$$

- ◆ Product bwn control and state
- ◆ Forward integration: how to make it **exact**?





Reformulation

Floating-base inverted pendulum (FIP)

Allow the ZMP to leave the contact area.¹

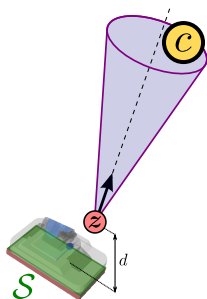


Figure : Friction constraint

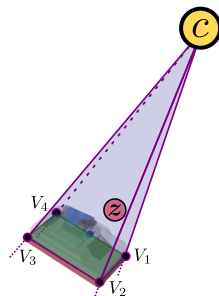
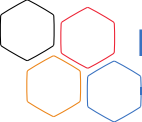


Figure : ZMP constraint

¹At heart, it is used to locate the central axis of the contact wrench [SB04]



Floating-base Inverted Pendulum

Equation of motion

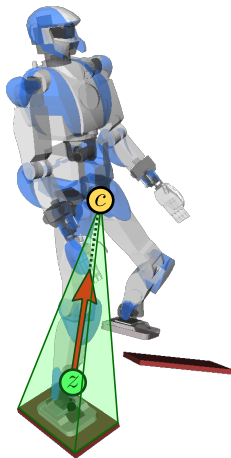
$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

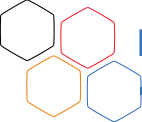
Constraints [CK17]

- Friction: $c - z \in \mathcal{C}$
- ZMP support cone:
 $\forall i, e_i \cdot (v_i - c) \times (z - v_i) \leq 0$

Assumptions

- Infinite torques
- Pendular mode





Properties of FIP model

Equation of motion

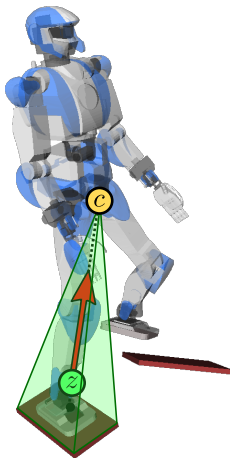
$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

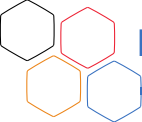
- Forward integration is **exact**:

$$c(t) = \alpha_0 e^{\omega t} + \beta_0 e^{-\omega t} + \gamma_0$$

- Capture Point is defined:

$$\xi = c + \frac{\dot{c}}{\omega} + \frac{\vec{g}}{\omega^2}$$



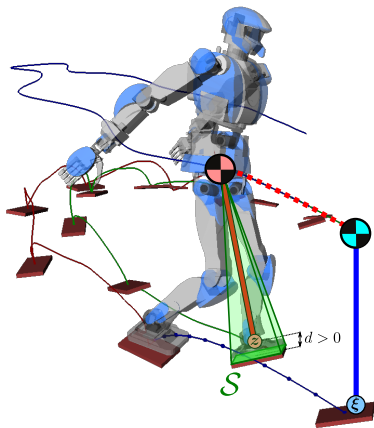


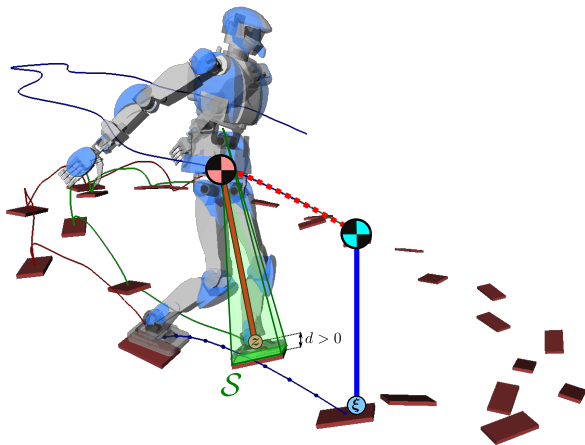
NMPC Optimization

- Runs at 30 Hz
- Adapts step timings
- FIP for forward integration
- Sometimes fails...

Linear-Quadratic Regulator

- Runs at 300 Hz
- Takes over when NMPC fails

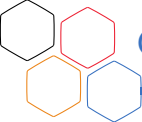




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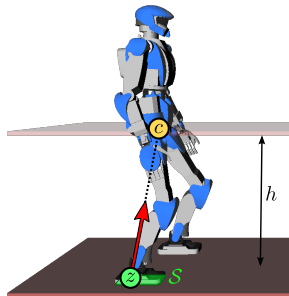


Conclusion



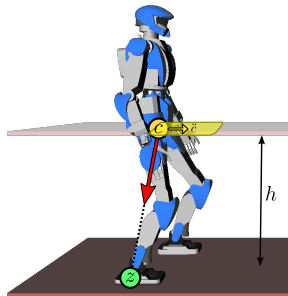
Conclusion

2D LIPM

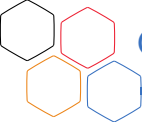


- Input: $z \in \mathcal{S}$
- Output: \ddot{c}

2D CART-table

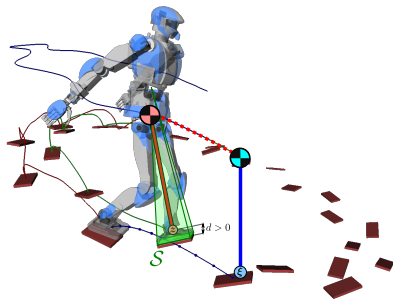


- Input: $\ddot{c} \in \omega^2(c - \mathcal{S}) + \vec{g}$
- Output: z



Conclusion

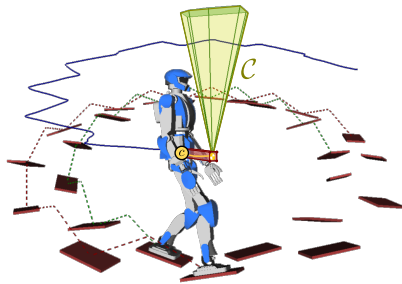
3D FIP [CK17]



Input: $z \in \mathcal{S}(c)$

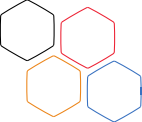
Output: \ddot{c}

3D COM-accel [CK16]



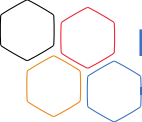
Input: $\ddot{c} \in \mathcal{C}(c)$

Output: z



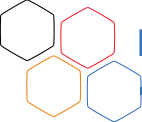
Thank you for your attention!





References I

- [Car17] Stéphane Caron. *My website*.
<https://scaron.info/teaching/>. 2017.
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