

DYNAMIC WALKING OVER ROUGH TERRAINS BY NONLINEAR PREDICTIVE CONTROL OF THE FLOATING-BASE INVERTED PENDULUM

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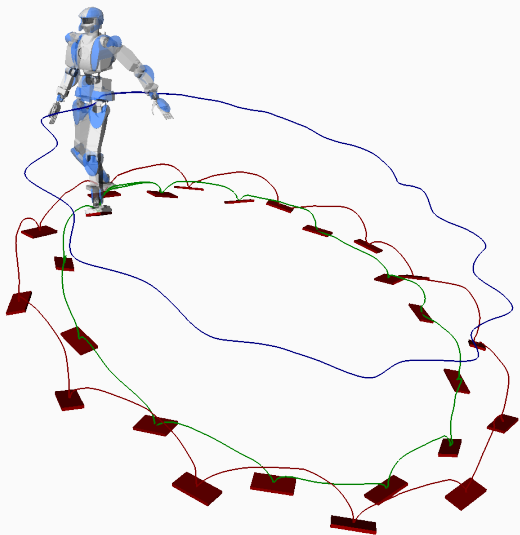


LIRMM

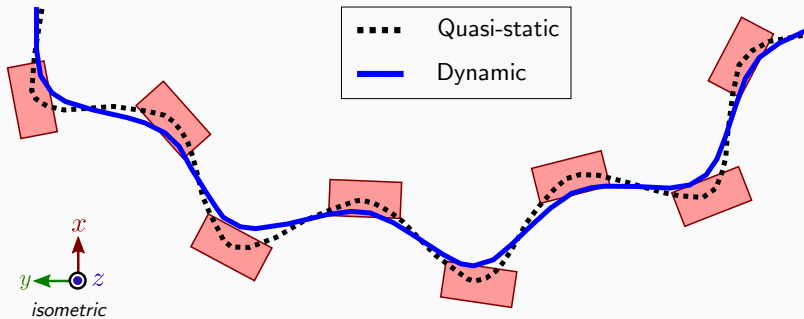


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GOAL



GOAL

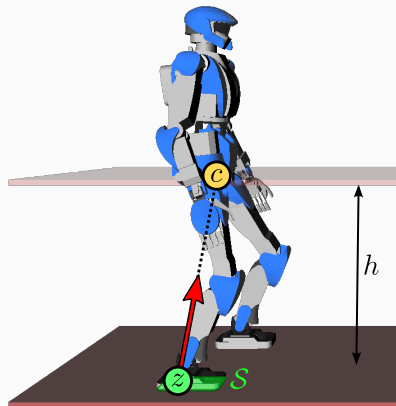


Equation of motion

$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

Feasibility conditions

- Constant: $\omega = \sqrt{g/h}$
- ZMP support area: $z \in \mathcal{S}$
- Friction?



Linear Inverted Pendulum

$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

Feasibility conditions

- Constant: $\omega = \sqrt{g/h}$
- ZMP support area: $z \in \mathcal{S}$
- Friction?

Inverted Pendulum

$$\ddot{c} = \lambda(c - z) + \vec{g}$$

Feasibility conditions

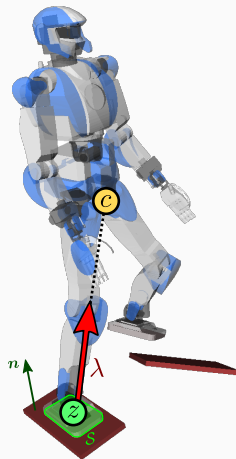
- Unilaterality: $\lambda \geq 0$
- ZMP support area: $z \in \mathcal{S}$
- Friction?

Equation of motion

$$\ddot{c} = \lambda(c - z) + \vec{g}$$

Feasibility conditions

- Unilaterality: $\lambda \geq 0$
- ZMP support area: $z \in \mathcal{S}$
- Friction?

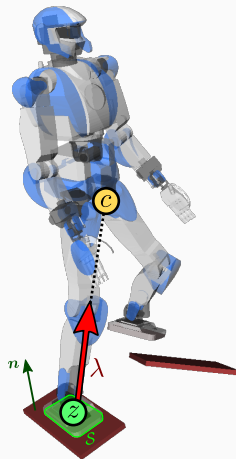


Equation of motion

$$\ddot{c} = \lambda(c - z) + \vec{g}$$

Feasibility conditions

- Unilaterality: $\lambda \geq 0$
- ZMP support area: $z \in \mathcal{S}$
- Friction?

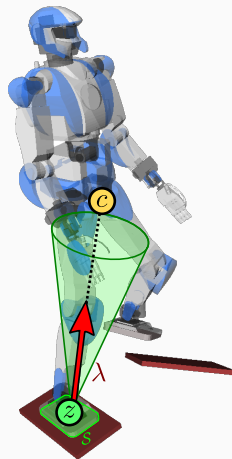


Equation of motion

$$\ddot{c} = \lambda(c - z) + \vec{g}$$

Feasibility conditions

- Unilaterality: $\lambda \geq 0$
- ZMP support area: $z \in \mathcal{S}$
- Friction: $c - z \in \mathcal{C}$

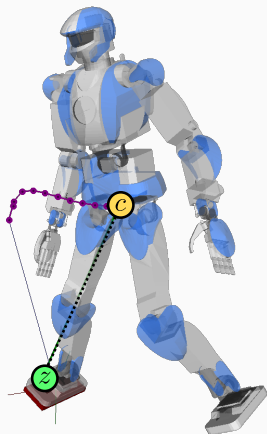


Equation of motion

$$\ddot{c} = \lambda(c - z) + \vec{g}$$

Forward integration¹

- Direct multiple shooting²
- Discretization: # of sample points, integration step
- Resolution of integrator?



¹See also Takasugi *et al.* (this session): "3D Walking and Skating..."

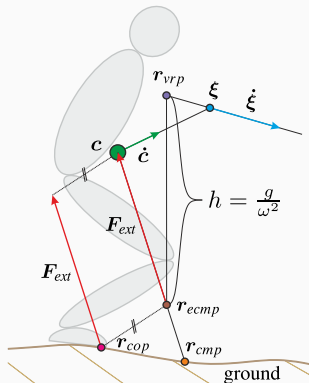
²Carpentier, Tonneau, Naveau, Stasse, and Mansard 2016.

Equation of motion

$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

Virtual Repellent Points

- The ZMP/eCMP/VRP² can leave the contact area
- Fwd integration is exact:
 $c(t) = \alpha e^{\omega t} + \beta e^{-\omega t} + \gamma$
- Feasibility conditions?



(Figure adapted from ²)

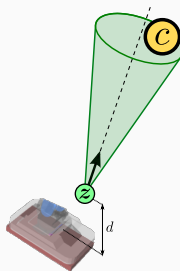
³Englsberger, Ott, and Albu-Schaffer 2015.

Equation of motion

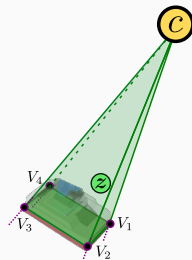
$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

Floating-base pendulum

- Floating ZMP (eCMP)
- Exact forward integration
- **New** feasibility condition



Friction cone



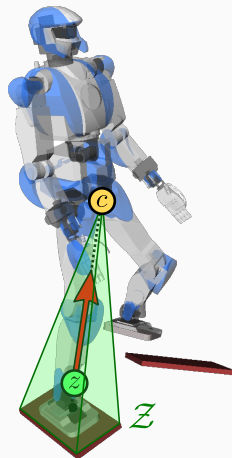
ZMP support cone

Equation of motion

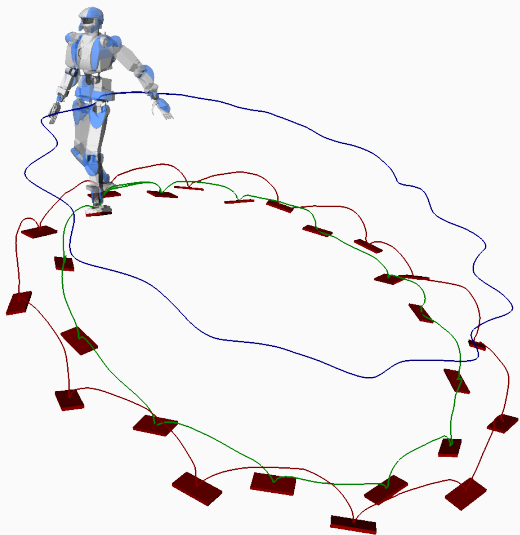
$$\ddot{c} = \omega^2(c - z) + \vec{g}$$

Feasibility conditions

- Constant: $\omega > 0$
- ZMP support cone: $z \in \mathcal{Z}$



GOAL

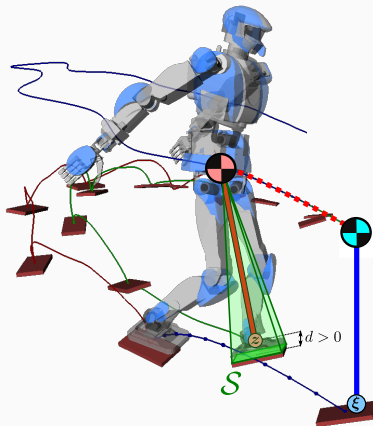


Nonlinear optimization...

- DMS over FIP model
- Adaptive step timings
- Runs at 30 Hz

... but significant failures

- Model is **nonconvex**
- Noise and delays in ZMP control / COM estimation
⇒ jumps in PO map



This communication:

Constrained LQ regulator

- Linear EoM + linearized ZMP cones = Quadratic Program
- Runs at 300 Hz, recovers locally from failures

⁴Caron and Mallein 2017.

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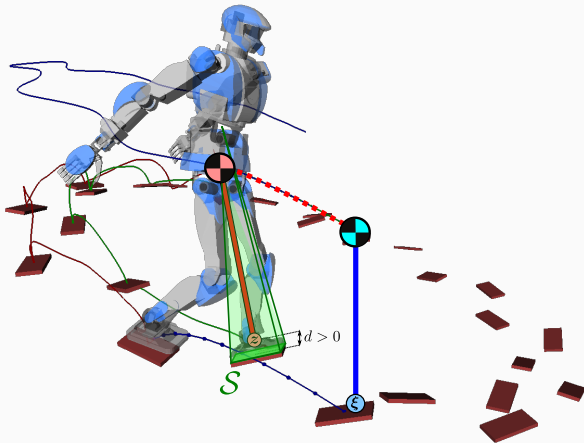
Next communication:³

Spoiler!

A *convexly-constrained* model: one global optimum, 1000 Hz
<https://scaron.info/research/3d-balance.html>

⁴Caron and Mallein 2017.

CHECK IT OUT!



<https://github.com/stephane-caron/dynamic-walking>

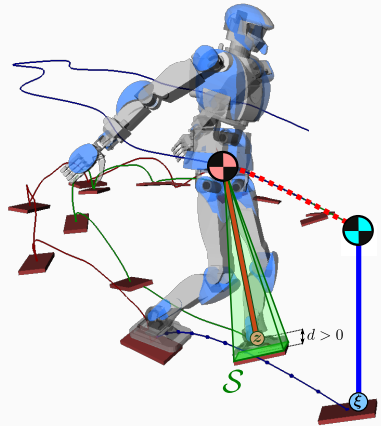
CONCLUSION

Floating-base Pendulum

- LTI model for 3D walking
- ZMP support area \Rightarrow cone




Nonlinear Predictive Control

- Can solve full problem
- Failures (nonconvexity)
- Recovery: constrained LQR



THANK YOU FOR YOUR ATTENTION!



-  Caron, Stéphane and Bastien Mallein (2017). "Balance control using both ZMP and COM height variations: A convex boundedness approach". working paper or preprint. URL: <https://scaron.info/research/3d-balance.html>.
-  Carpentier, J., S. Tonneau, M. Naveau, O. Stasse, and N. Mansard (2016). "A versatile and efficient pattern generator for generalized legged locomotion". In: *2016 IEEE International Conference on Robotics and Automation (ICRA)*, pp. 3555–3561.
-  Engelsberger, Johannes, Christian Ott, and Alin Albu-Schaffer (2015). "Three-dimensional bipedal walking control based on divergent component of motion". In: *IEEE Transactions on Robotics* 31.2, pp. 355–368.